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# Introduction to Robotics

## Lecture 5

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Technical Aspects of Multimodal Systems

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Introduction

Coordinate systems

Kinematic Equations

Robot Description

Inverse Kinematics for Manipulators

Differential motion with homogeneous transformations

Jacobian

- Jacobian of a Manipulator

- Singular Configurations

Trajectory planning

Trajectory generation

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Principles of Walking





# Outline (cont.)

Jacobian

Introduction to Robotics

Robot Control

Task-Level Programming and Trajectory Generation

Task-level Programming and Path Planning

Task-level Programming and Path Planning

Architectures of Sensor-based Intelligent Systems

Summary

Conclusion and Outlook





## Definition

- ▶ A Jacobian-matrix is a multidimensional representation of partial derivatives.
- ▶ The Jacobian of a manipulator links the joint velocities with the cartesian velocity of the TCP.
- ▶ The Jacobian matrix depends on the current state of the robot joints.

# Jacobian of a Manipulator (cont.)

- ▶ Consider an n-link manipulator with joint variables  $q_1, q_2, \dots, q_n$ .
- ▶ Define  $q = [q_1, q_2, \dots, q_n]^T$
- ▶ Let the transformation from base to end-effector frame be:

$$\mathcal{T} = \begin{bmatrix} R_n^0(q) & o(q) \\ 0 & 1 \end{bmatrix} \quad (52)$$

- ▶ We define  $\omega_n^0$  to be the angular velocity of the end-effector
- ▶ The linear velocity of the end-effector is  $v_n^0$
- ▶ The **Jacobian** matrix consists of two components, that solve the following equations:

$$v_n^0 = J_v \dot{q} \quad \text{and} \quad \omega_n^0 = J_w \dot{q}$$

## The manipulator Jacobian

$$J := \begin{bmatrix} J_v \\ J_w \end{bmatrix}$$

We define the body velocity of the endeffector:

$$\xi := \begin{bmatrix} v_n^0 \\ \omega_n^0 \end{bmatrix} := \begin{bmatrix} {}^T d_x \\ {}^T d_y \\ {}^T d_z \\ {}^T \delta_x \\ {}^T \delta_y \\ {}^T \delta_z \end{bmatrix} \quad \xi = J\dot{q}$$

## Revolute joints

If the  $i^{\text{th}}$  joint is revolute, the axis of rotation is given by  $z_{i-1}$ .

Let  $\omega_{i-1,i}^{i-1}$  represent the angular velocity of the link  $i$  w.r.t. the frame  $i-1$ .

Then, we have: 
$$\omega_{i-1,i}^{i-1} = \dot{q}_i z_{i-1}^{i-1}$$

## Prismatic joints

If the  $i^{\text{th}}$  joint is prismatic, the motion of frame  $i$  relative to frame  $i-1$  is a translation.

Then, we have: 
$$\omega_{i-1,i}^{i-1} = 0$$

# Angular Velocity Jacobian (cont.)

Overall angular velocity:

$$\omega_{0,n}^0 = \omega_{0,1}^0 + R_1^0 \omega_{1,2}^1 + \dots + R_{n-1}^0 \omega_{n-1,n}^{n-1} \quad (53)$$

We get:

$$\omega_{0,n}^0 = p_1 \dot{q}_1 z_0^0 + p_2 \dot{q}_2 R_1^0 z_1^1 + \dots + p_n \dot{q}_n R_{n-1}^0 z_{n-1}^{n-1} \quad (54)$$

$$= p_1 \dot{q}_1 z_0^0 + p_2 \dot{q}_2 z_1^0 + \dots + p_n \dot{q}_n z_{n-1}^0 \quad (55)$$

where:

$$p_i = \begin{cases} 0 & \text{if } i \text{ is prismatic} \\ 1 & \text{if } i \text{ is revolute} \end{cases} \quad (56)$$



## The complete Jacobian

$$\begin{bmatrix} v_n^0 \\ \omega_n^0 \end{bmatrix} = \begin{bmatrix} J_v \\ J_w \end{bmatrix} \dot{q} \quad (57)$$

## The Angular Velocity Jacobian

$$J_w = [p_1 z_0^0 \quad p_2 z_1^0 \quad \dots \quad p_n z_{n-1}^0] \quad (58)$$

(Hint:  $J_w$  is a  $3 \times n$  matrix; due to matrix multiplication rules the representation is equal to those on the last slide.)



The linear velocity of the end effector is:  $\dot{o}_n^0$

By the chain rule of differentiation:

$$\dot{o}_n^0 = \frac{\delta o_n^0}{\delta q_1} \dot{q}_1 + \frac{\delta o_n^0}{\delta q_2} \dot{q}_2 + \dots + \frac{\delta o_n^0}{\delta q_n} \dot{q}_n \quad (59)$$

therefore the linear part of the Jacobian is:

$$J_v = \begin{matrix} \frac{\delta o_n^0}{\delta q_1} & \frac{\delta o_n^0}{\delta q_2} & \dots & \frac{\delta o_n^0}{\delta q_n} \end{matrix} \quad (60)$$

Every prismatic joint influences the velocity of the endeffector depending on:

- ▶ the current linear velocity of the joint ( $\dot{d}_i$ )
- ▶ the current orientation of the z-axis of the joint ( $z_{i-1}$ )
  - ▶ depending on  $q$

$$\dot{o}_n^0 = \dot{d}_i z_{i-1} \quad (61)$$

Therefore:

$$J_{v_i} = \frac{\delta o_n^0}{\delta q_n} = z_{i-1} \quad (62)$$

Every revolute joint influences the velocity of the end-effector depending on:

- ▶ the current angular velocity of the joint ( $\dot{q}_i$ )
- ▶ the current orientation of the z-axis of the joint ( $z_{i-1}$ )
- ▶ the current vector from the joint origin  $o_{i-1}$  to the end-effector
  - ▶ the two latter depending on  $q$

The linear velocity of the end-effector is of form:

$$\omega \times r$$

with  $\omega = \dot{q}_i z_{i-1}$  and  $r = o_n^0 - o_{i-1}^0$

Therefore:

$$J_{v_i} = \frac{\delta o_n^0}{\delta q_n} = z_{i-1} \times (o_n^0 - o_{i-1}^0) \quad (63)$$

$$J := \begin{bmatrix} J_v \\ J_w \end{bmatrix}$$

$$J_v = [J_{v_1} \quad J_{v_2} \quad J_{v_n}] \quad \text{with} \quad (64)$$

$$J_{v_i} = \begin{cases} z_{i-1} & \text{if } i \text{ is prismatic} \\ z_{i-1} \times (o_n^0 - o_{i-1}^0) & \text{if } i \text{ is revolute} \end{cases} \quad (65)$$

and  $J_w = [J_{w_1} \quad J_{w_2} \quad J_{w_n}]$  with (66)

$$J_{w_i} = \begin{cases} 0 & \text{if } i \text{ is prismatic} \\ z_{i-1} & \text{if } i \text{ is revolute} \end{cases} \quad (67)$$

# Computing the final Jacobian (cont.)

## Target

Compute  $z_i$  and  $o_i$ .

- ▶  $z_i$  is equal to the first three elements of the 3rd column of matrix  ${}^0T_i$
- ▶  $o_i$  is equal to the first three elements of the 4th column of matrix  ${}^0T_i$

${}^0T_i$  has to be computed for every joint.

Consider a Manipulator with 6 DOFs:

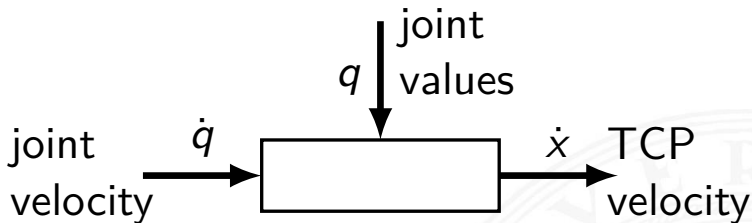
$$T_6 = A_1 A_2 A_3 A_4 A_5 A_6$$

the Jacobian is:

$$\begin{bmatrix} T_6 d_x \\ T_6 d_y \\ T_6 d_z \\ T_6 \delta_x \\ T_6 \delta_y \\ T_6 \delta_z \end{bmatrix} = J_{6 \times 6} \begin{bmatrix} dq_1 \\ dq_2 \\ dq_3 \\ dq_4 \\ dq_5 \\ dq_6 \end{bmatrix}$$

$$\dot{\mathbf{x}} = J(\mathbf{q}) \dot{\mathbf{q}}$$

In case of a 6-DOF manipulator, we get a  $6 \times 6$  matrix.



## Question

Is the Jacobian invertible?

If it is, then:

$$\dot{q} = J^{-1}(q)\dot{x}$$

$\implies$  to move the the end-effector of the robot in Cartesian Space with a certain velocity.



For most manipulators there exist values of  $\mathbf{q}$  where the Jacobian gets **singular**.

## Singularity

$$\det J = 0 \implies J \text{ is not invertible}$$

Such configurations are called **singularities** of the manipulator.

Two Main types of Singularities:

- ▶ Workspace boundary singularities
- ▶ Workspace internal singularities

# Singular Configurations – Workarounds

- ▶ generally only for 6-DOF manipulators the Jacobian is invertible
  - ▶ there are workarounds for other types of manipulators
- $n < 6$  manually restrict the DOF of the end-effector  
⇒ square Jacobian matrix.

Example:

$$\begin{bmatrix} T_6 d_x \\ T_6 d_y \end{bmatrix} = J_{2 \times 2} \begin{bmatrix} dq_1 \\ dq_2 \end{bmatrix}$$

for a 2-joint planar manipulator

- $n > 6$  use the pseudoinverse of  $J$

$$A^+ = (A^T \cdot A)^{-1} \cdot A^T, \text{ linear independent columns} \quad (68)$$

$$A^+ = A^T \cdot (A^T \cdot A)^{-1}, \text{ linear independent rows} \quad (69)$$

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